# Evaluation of GPS in Orthometric Heights Determination in Khartoum State (Sudan) 

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#### Abstract

Levelling is the usual technique used to determine difference in height between ground points. Nowadays Global Positioning System (GPS) provides a quick modern technology to determine this difference. Because the datum surfaces are different in both techniques, different results may be expected. In this research work, difference in heights between numbers of points, in Khartoum State, were carried out using both ordinary levelling (in which Geoid is the reference datum) and GPS techniques (in which Ellipsoid is the reference datum). Results obtained showed that GPS data can be used directly to produce contour map up to $1: 100,000$ map scale with 25 m interval. Results also assisted to determine the Geoid undulation in the area. Moreover, GPS data can be improved using EGM2008 Gravitational model, to be suitable for $\mathbf{1 : 2 5 , 0 0 0}$ contour map scales, with 6.25 m contour interval.


Keywords- GPS, Ordinary and Geodetic Levelling Orthometric Height and Geoid Undulation

## I. INTRODUCTION

Number of quantities has to be measured in usual survey works. These quantities may be bearings, angles, or distances (horizontal, vertical or inclined). Reduction of theses values leads to determination of relative position of the points.

Levelling is the name given to the process of measuring the difference in elevation between two or more points. The heights of points relative to a chosen surface are known as reduced levels of these points. Reference surface is usually known as a datum.

In engineering surveying, leveling has many applications and is used in all stages in construction projects from the initial site survey through to the final setting out [2].

Levelling process can be carried out using different survey equipments and techniques. It may be precise; when precise optical or digital levels are used, or it may be ordinary; when using ordinary optical, automatic or digital levels. Moreover it can be carried out trigonometrically or barometrically.

## II. ORDINARY AND GEODETIC LEVELLING

In short distances, difference in level between two points can easily be determined by setting a staff vertically in each point. Then, constructing a horizontal line using optical or digital level. Difference in the intersection points of the
horizontal line with both staves produce the difference in level between these ground points Fig. 1. This technique is simply known as ordinary leveling [4].

In long distances, when geoid undulation of the earth has to be taken into account, direct levelling doesn't solve the problem and it will be more complicated. This is so because horizontal line does not solve the problem directly. Levelling technique taking the geoid undulation into account is usually known as geodetic levelling.


Fig. 1: Ordinary Levelling

## III. GEOID AND ELLIPSOID

The Geoid is an equipotential of the gravity force surface located approximately at mean sea level, which is everywhere perpendicular to the direction of gravity. Orthometric levelling is the term used when using geoid as a reference datum. Because of variations in the earth mass distribution, the geoid has an irregular shape [3].

Regular shape can be approximated by the Ellipsoid. Ellipsoid is a mathematical surface obtained by revolving an ellipse about its minor axis. Levelling based on taking the geoid as a reference datum is then termed Geodetic levelling. The dimensions of the ellipse are selected to give a best fit of the ellipsoid to the geoid over a large area, and are based upon surveys made in the area.

A two-dimensional view which illustrates conceptually the geoid and ellipsoid is shown in Fig. 2. As illustrated, the geoid contains non uniform undulations, and is therefore not readily defined mathematically. Ellipsoids, which
approximate the geoid and can be defined mathematically, are therefore used to compute positions of widely spaced points that are located.


Fig. 2: Geoid and ellipsoid surfaces

Historically, Clarke1880 ellipsoid was used as a reference datum -local datum- for long time in Sudan (Termed technically Adindan Sudan). Recently, because of the wide spread use of global positioning system (GPS), world geodetic system (WGS1984) becomes an available alternative.

## IV. GLOBAL POSITIONING SYSTEM

Global Positioning System (GPS) was developed by the (U.S.A) to determine coordinates of points. Global positioning system consists of three components; these are space segment, control segment and user segment. Every component has its essential role in improving the positioning accuracy [1].

In this system, ground control receivers monitor the signals transmitted from a set of space segment (satellites). The received signals are used to solve for the coordinates of the position where the receivers are located. The GPS satellites are configured to provide the users with capability of positioning fixing.

Ground receiver equipments consist of two major units, antenna and units of analysis. The antenna is designed to receive the waves that come from satellites. Unit of analysis is linked to Antenna to analyze the data received by Antenna.

Global Positioning System (GPS) provides number of advantages e.g., the comprehensive coverage during the $24-$ hour, comprehensive coverage of spatial locations of each hemisphere, does not need to monitor the use of direct and traditional methods, link all the points of the coordinates of a global uniform and provide a great deal of time in the work of the main connecting points of the major projects.

Because of its high precision measurements, its uses not confined to the process of identifying the exact locations of the vessels at sea and ground control point locations, but many geodetic applications and uses of the system became an active role to play effective applications in the areas of civil engineering such as civil engineering, surveying, aerial surveys, environmental engineering, engineering of airports, air navigation, geodetic, geophysical applications and modern systems such as geographic information systems (GIS) etc.


Fig. 3: GPS Components

## V. EARTH GRAVITATIONAL MODEL (2008)

The official EGM2008 has been publicly released by the U.S. National Geospatial-Intelligence Agency (NGA) EGM Development Team. This gravitational model is complete to spherical harmonic degree and order 2159 , and contains additional coefficients extending to degree 2190 and order 2159. The WGS 84 constants used to define the reference ellipsoid, and the associated normal gravity field, to which the geoid undulations are referenced are:

- $a=6378137.00 \mathrm{~m}$ (semi-major axis of WGS 84 ellipsoid),
- $f=1 / 298.257223563$ (flattening of WGS 84 ellipsoid),
- $G M=3.986004418 \times 1014 \mathrm{~m} 3 \mathrm{~s}-2$ (Product of the Earth's mass and the Gravitational Constant),
- $\omega=7292115 \mathrm{x}$ 10-11 radians/sec (Earth's angular velocity).

All synthesis software, coefficients, and pre-computed geoid grids, assume a tide free system, as far as permanent tide is concerned [6].

Note that the harmonic synthesis software applies a constant, zero-degree term of -41 cm to all geoid undulations computed using EGM2008 with the height anomaly to geoid undulation correction model (also provided). Similarly, all pre-computed geoid undulations incorporate this constant zero-degree term. This term converts geoid undulations that are intrinsically referenced to an ideal mean-earth ellipsoid into undulations that are referenced to WGS 84. The value of -41 cm derives from a mean-earth ellipsoid for which the estimated parameters in the Tide Free system are:

$$
\mathrm{a}=6378136.58 \mathrm{~m} \text { and } 1 / \mathrm{f}=298.257686 .
$$



Fig. 4: Gravitational Model EGM2008

## VI. MEASUREMENTS AND RESULTS

In this research work, ordinary levelling was carried out for 49 points of about one kilometer interval along 50 kilometers in Khartoum state (Sudan). Automatic level was used to do the job. Level line was started at a known benchmark and end at another one. Observations were reduced and adjusted. Orthometric heights (H) were obtained on Adindan Sudan reference datum as shown in Table 1 below.

Real Time GPS observations were carried out along the same line. Observations were processed and adjusted to compute ellipsoidal height (h) of all points. Results were obtained as illustrated in the table below.

Comparison between orthometric height of points and ellipsoidal heights of the same points can be carried out by computing the differences $(\mathrm{N})$ between both results as shown in Table 1 below. These differences represent the geoid ellipsoid separation in the area.

Table 1: Geoid Ellipsoid separation (N) i.e. (Errors in GPS heights)

| Point | Ellepoidal Height(h) (m) | $\begin{aligned} & \text { Ortometric } \\ & \text { Hieght(H) } \\ & (\mathrm{m}) \end{aligned}$ | $\begin{gathered} \mathbf{N} \\ (\mathbf{m}) \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| 1 | 386.662 | 382.935 | 3.727 |
| 2 | 387.588 | 383.797 | 3.791 |
| 3 | 387.772 | 384.117 | 3.655 |
| 4 | 388.761 | 385.13 | 3.631 |
| 5 | 389.445 | 385.862 | 3.583 |
| 6 | 388.974 | 385.472 | 3.502 |
| 7 | 390.653 | 386.967 | 3.686 |
| 8 | 390.406 | 386.707 | 3.699 |
| 9 | 389.78 | 386.172 | 3.608 |
| 10 | 389.43 | 386.157 | 3.273 |
| 11 | 389.469 | 386.202 | 3.267 |
| 12 | 389.721 | 386.438 | 3.283 |
| 13 | 390.092 | 386.785 | 3.307 |
| 14 | 389.263 | 385.945 | 3.318 |


| 15 | 389.46 | 386.12 | 3.34 |
| :---: | :---: | :---: | :---: |
| 16 | 390.072 | 386.713 | 3.359 |
| 17 | 390.318 | 386.958 | 3.36 |
| 18 | 391.613 | 388.225 | 3.388 |
| 19 | 393.554 | 390.108 | 3.446 |
| 20 | 396.098 | 392.587 | 3.511 |
| 21 | 398.293 | 394.757 | 3.536 |
| 22 | 399.01 | 395.472 | 3.538 |
| 23 | 399.472 | 395.947 | 3.525 |
| 24 | 398.838 | 395.324 | 3.514 |
| 25 | 399.095 | 395.554 | 3.541 |
| 26 | 400.235 | 396.719 | 3.516 |
| 27 | 399.903 | 396.347 | 3.556 |
| 28 | 400.268 | 396.666 | 3.602 |
| 29 | 398.081 | 394.464 | 3.617 |
| 30 | 395.394 | 391.711 | 3.683 |
| 31 | 393.896 | 390.263 | 3.633 |
| 32 | 395.277 | 391.571 | 3.706 |
| 33 | 396.884 | 393.224 | 3.66 |
| 34 | 398.659 | 394.964 | 3.695 |
| 35 | 399.075 | 395.52 | 3.555 |
| 36 | 398.962 | 395.302 | 3.66 |
| 37 | 401.6 | 397.928 | 3.672 |
| 38 | 405.936 | 402.263 | 3.673 |
| 39 | 407.63 | 403.978 | 3.652 |
| 40 | 410.558 | 406.843 | 3.715 |
| 41 | 410.698 | 406.98 | 3.718 |
| 42 | 407.92 | 404.245 | 3.675 |
| 43 | 404.546 | 401.823 | 2.723 |
| 44 | 401.535 | 397.809 | 3.726 |
| 45 | 401.214 | 397.449 | 3.765 |
| 46 | 404.248 | 400.449 | 3.799 |
| 47 | 407.558 | 403.749 | 3.809 |
| 48 | 406.925 | 403.191 | 3.734 |
| 49 | 405.875 | 402.161 | 3.714 |
| Average $\mathrm{N}=3.564 \mathrm{~m}$ |  |  |  |
| Root Mean Square Error of $\mathrm{N}=3.569 \mathrm{~m}$ |  |  |  |

The average difference between orthometric heights and ellipsoidal heights in the study area was found to be 3.564 m with 3.569 m root mean square error.

Practically, ellipsoidal heights can be reduced to orthometric heights if geoid ellipsoid separation (N) is known.

In this work, EGM2008 geodetic model was used to compute geoid ellipsoid separation (undulation). Reduced geoid andulations for the observed points are listed in the following Table 2.

Table 2: Reduced EGM2008 geoid ellipsoid separation (N)

| Point | Latitude | Longitude | $\begin{aligned} & \text { EGM2 } \\ & \mathbf{0 0 8 ( N )} \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| 1 | $15^{\circ} 35{ }^{\prime} 28.28098{ }^{\prime \prime} \mathrm{N}$ | 32 ${ }^{\circ} 36{ }^{\prime} 56.642922^{\prime \prime}$ E | 2.387 |
| 2 | $15^{\circ} 35^{\prime} 28.48429{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 37{ }^{\prime} 30.22032^{\prime \prime}$ E | 2.381 |
| 3 | $15^{\circ} 35^{\prime} 28.52582{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 38^{\prime} 03.79984^{\prime \prime}$ E | 2.376 |
| 4 | $15^{\circ} 35{ }^{\prime} 28.56041^{\prime \prime} \mathrm{N}$ | $32^{\circ} 38^{\prime} 37.37892^{\prime \prime}$ E | 2.370 |
| 5 | $15^{\circ} 35^{\prime} 28.59265^{\prime \prime} \mathrm{N}$ | $32^{\circ} 39^{\prime} 10.95841^{\prime \prime}$ E | 2.364 |
| 6 | $15^{\circ} 35^{\prime} 28.62923$ " N | $32^{\circ} 39^{\prime} 44.53721^{\prime \prime}$ E | 2.358 |
| 7 | $15^{\circ} 35^{\prime} 42.33917^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 05.03774{ }^{\prime \prime}$ E | 2.364 |
| 8 | $15^{\circ} 36^{\prime} 14.88522^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 04.98496^{\prime \prime}$ E | 2.387 |
| 9 | $15^{\circ} 36{ }^{\prime} 45.64159{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 04.91679{ }^{\prime \prime}$ E | 2.409 |
| 10 | $15^{\circ} 37^{\prime} 17.46176^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 04.95775^{\prime \prime}$ E | 2.431 |
| 11 | $15^{\circ} 37{ }^{\prime} 50.00769^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 04.91674^{\prime \prime}$ E | 2.453 |
| 12 | $15^{\circ} 388^{\prime 2} 2.553833^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40 \cdot 04.88659^{\prime \prime}$ E | 2.474 |
| 13 | $15^{\circ} 388^{\prime} 55.09950{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 04.89251{ }^{\prime \prime}$ E | 2.495 |
| 14 | $15^{\circ} 39^{\prime} 25.18699^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 16.93145^{\prime \prime}$ E | 2.512 |
| 15 | $15^{\circ} 39^{\prime} 57.21745{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 22.77125^{\prime \prime}$ E | 2.531 |
| 16 | $15^{\circ} 40^{\prime} 29.30227^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 28.40930^{\prime \prime}$ E | 2.550 |
| 17 | $15^{\circ} 41^{\prime} 01.39351^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 34.00758^{\prime \prime}$ E | 2.568 |
| 18 | $15^{\circ} 41^{\prime} 33.48313^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 39.61126^{\prime \prime}$ E | 2.586 |
| 19 | $15^{\circ} 42^{\prime} 05.53982^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 45.41510{ }^{\prime \prime}$ E | 2.604 |
| 20 | $15^{\circ} 42^{\prime} 37.65666{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 50.80197^{\prime \prime}$ E | 2.621 |
| 21 | $15^{\circ} 43^{\prime} 09.84494{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 55.77394^{\prime \prime}$ E | 2.637 |
| 22 | $15^{\circ} 43$ '42.22209" N | $32^{\circ} 40{ }^{\prime} 56.77734^{\prime \prime}$ E | 2.655 |
| 23 | $15^{\circ} 44^{\prime} 14.25138{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 50.82525{ }^{\prime \prime}$ E | 2.672 |
| 24 | $15^{\circ} 44^{\prime} 46.26347^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 44.76618^{\prime \prime}$ E | 2.690 |
| 25 | $15^{\circ} 45^{\prime} 18.27536{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 38.70319{ }^{\prime \prime}$ E | 2.716 |
| 26 | $15^{\circ} 45^{\prime} 50.28918^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 32.65072^{\prime \prime}$ E | 2.732 |
| 27 | $15^{\circ} 46^{\prime} 22.30340{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 26.60186^{\prime \prime}$ E | 2.546 |
| 28 | $15^{\circ} 47^{\prime} 58.34820{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 08.461811^{\prime \prime}$ E | 2.790 |
| 29 | $15^{\circ} 48^{\prime} 30.36066{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 02.40077^{\prime \prime}$ E | 2.802 |
| 30 | $15^{\circ} 49^{\prime} 02.37182^{\prime \prime} \mathrm{N}$ | $32^{\circ} 39^{\prime} 56.33266^{\prime \prime}$ E | 2.815 |
| 31 | $15^{\circ} 49^{\prime} 34.38611^{\prime \prime} \mathrm{N}$ | $32^{\circ} 39^{\prime} 50.28272^{\prime \prime}$ E | 2.827 |
| 32 | $15^{\circ} 50^{\prime} 06.40397{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 39^{\prime} 44.25410{ }^{\prime \prime}$ E | 2.838 |
| 33 | $15^{\circ} 50^{\prime} 38.42119{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 39^{\prime} 38.21771{ }^{\prime \prime}$ E | 2.848 |
| 34 | $15^{\circ} 511^{\prime} 10.44067{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 39^{\prime} 32.19469^{\prime \prime}$ E | 2.857 |
| 35 | $15^{\circ} 51^{\prime} 42.45744{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 39^{\prime} 26.15935{ }^{\prime \prime}$ E | 2.866 |
| 36 | $15^{\circ} 52^{\prime} 14.47629^{\prime \prime} \mathrm{N}$ | $32^{\circ} 39^{\prime} 20.13635^{\prime \prime}$ E | 2.874 |
| 37 | $15^{\circ} 52^{\prime} 46.49807^{\prime \prime} \mathrm{N}$ | $32^{\circ} 39^{\prime} 14.12822^{\prime \prime}$ E | 2.882 |
| 38 | $15^{\circ} 53^{\prime} 18.51532^{\prime \prime} \mathrm{N}$ | $32^{\circ} 39^{\prime} 08.09388^{\prime \prime}$ E | 2.888 |
| 39 | $15^{\circ} 53 ' 50.68458{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 39^{\prime} 04.20829^{\prime \prime}$ E | 2.894 |
| 40 | $15^{\circ} 54^{\prime} 22.31993{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 39^{\prime} 12.06631^{\prime \prime}$ E | 2.898 |
| 41 | $15^{\circ} 54^{\prime} 53.89724^{\prime \prime} \mathrm{N}$ | $32^{\circ} 39^{\prime} 20.20674^{\prime \prime}$ E | 2.902 |
| 42 | $15^{\circ} 55^{\prime} 25.47769^{\prime \prime} \mathrm{N}$ | $32^{\circ} 39^{\prime} 28.33516^{\prime \prime}$ E | 2.877 |
| 43 | $15^{\circ} 55^{\prime} 57.06144{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 39^{\prime} 36.44949{ }^{\prime \prime}$ E | 2.881 |
| 44 | $15^{\circ} 56^{\prime} 28.64441{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 39^{\prime} 44.568889^{\prime \prime}$ E | 2.884 |
| 45 | $15^{\circ} 57{ }^{\prime} 00.22799{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 39^{\prime} 52.68608^{\prime \prime}$ E | 2.887 |
| 46 | $15^{\circ} 57{ }^{\prime} 31.80978{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 00.81011{ }^{\prime \prime}$ E | 2.891 |
| 47 | $15^{\circ} 588^{\prime} 03.39026^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 08.93919{ }^{\prime \prime}$ E | 2.894 |
| 48 | $15^{\circ} 588^{\prime} 34.97430{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} 17.05577{ }^{\prime \prime}$ E | 2.898 |
| 49 | $15^{\circ} 59^{\prime} 06.56038{ }^{\prime \prime} \mathrm{N}$ | $32^{\circ} 40^{\prime} \mathbf{2 5 . 1 6 3 9 0}{ }^{\prime \prime}$ E | 2.901 |

From the results obtained above, average separation can be computed to be 2.673 m .
Ortometric heights are then calculated by adding geodetic heights (H) to geoid separation (N) using the following equation:

$$
\begin{equation*}
H=h+N \tag{1}
\end{equation*}
$$

Where,
$H$ represents orthometric height, $h$ represents Ellipsoidal height and $N$ represents geoid ellipsoid undulation.

Computed Orhtometric heights obtained are listed as demonstrated in Table 3.

Finally, the actual orthometric heights were compared with those orthometric reduced from GPS observations by computing geoid ellipsoid separation (undulation) the error difference. The following Table 3 illustrates results.

Table 3: Difference between reduced and actual orthometric heights (errors)

| Point | Computed Ortometric Hieght(H) h+N (m) | Actual Ortometric Hieght(H) (m) | Difference (m) |
| :---: | :---: | :---: | :---: |
| 1 | 384.2753 | 382.935 | 1.340 |
| 2 | 385.2066 | 383.797 | 1.410 |
| 3 | 385.3961 | 384.117 | 1.279 |
| 4 | 386.3908 | 385.13 | 1.261 |
| 5 | 387.0807 | 385.862 | 1.219 |
| 6 | 386.6159 | 385.472 | 1.144 |
| 7 | 388.2888 | 386.967 | 1.322 |
| 8 | 388.0186 | 386.707 | 1.312 |
| 9 | 387.371 | 386.172 | 1.199 |
| 10 | 386.9992 | 386.157 | 0.842 |
| 11 | 387.0162 | 386.202 | 0.814 |
| 12 | 387.2467 | 386.438 | 0.809 |
| 13 | 387.5966 | 386.785 | 0.812 |
| 14 | 386.7506 | 385.945 | 0.806 |
| 15 | 386.9286 | 386.12 | 0.809 |
| 16 | 387.522 | 386.713 | 0.810 |
| 17 | 387.7497 | 386.958 | 0.792 |
| 18 | 389.0269 | 388.225 | 0.802 |
| 19 | 390.9505 | 390.108 | 0.843 |
| 20 | 393.4774 | 392.587 | 0.890 |
| 21 | 395.6556 | 394.757 | 0.899 |
| 22 | 396.3554 | 395.472 | 0.883 |
| 23 | 396.7997 | 395.947 | 0.853 |
| 24 | 396.1483 | 395.324 | 0.824 |
| 25 | 396.3791 | 395.554 | 0.825 |
| 26 | 397.5028 | 396.719 | 0.784 |
| 27 | 397.3569 | 396.347 | 1.010 |
| 28 | 397.4776 | 396.666 | 0.812 |
| 29 | 395.2786 | 394.464 | 0.815 |
| 30 | 392.5786 | 391.711 | 0.868 |
| 31 | 391.0691 | 390.263 | 0.807 |
| 32 | 392.4393 | 391.571 | 0.868 |
| 33 | 394.0361 | 393.224 | 0.812 |
| 34 | 395.8017 | 394.964 | 0.838 |



Note that, the accuracy estimation based on the criteria of the root mean squire error RMSE, which can be computed as:

$$
\begin{equation*}
R M S E=\sqrt{\frac{\sum(\bar{x}-x)^{2}}{n}} \tag{2}
\end{equation*}
$$

Where,
$x$ is the actual quantity,
$x$ is the measured quantity, and
$n$ is the number of quantities.
The root mean square errors of the measured points was computed and tabulated in Table 2.

From Table 3 above the mean difference was found to be 0.891 m , where, 0.922 m root mean square error was obtained.

Fig. 5 below show diagrammatically observed points distributed along the chainage line against heights.


Fig. 5: Orthometric and Ellipsoidal heights

## VII. CONCLUSION

Regarding the study area, and by referring to observation carried out and results obtained above, it can directly conclude that:
i. In the study area, error of about 3.569 m in orthometric heights can be expected when utilizing GPS directly in levelling applications. This result leads to ability of using GPS directly in levelling observation to produce maps at scale of about 1:80,000 (and smaller) with 25 m contour interval, according to Sudan map specification.
ii. Orthometric heights can be reduced from GPS observation by obtaining the geoid ellipsoid separation (geoid undulation) with aid of one of available geoid models. This can easily be done by subtracting resultant undulations from GPS heights.
iii. Applying EGM2008 geoid model to GPS observation in Khartoum state can successfully produce results estimated with 0.922 m accuracy in orthometric height. This accuracy in height can be used to produce contour maps at scales $1: 18,000$ and smaller according to Sudan authority specification. These maps can be plotted with 2 m interval.

## VIII. RECOMMENDATIONS

This research work is oriented to study the accuracy of GPS in height determination in Khartoum state. Also to evaluate the improvements in heights that can be obtained when using EGM2008 geodetic model in geoid ellipsoid separation. Further studies can be oriented to:
i. Integrating number of local observed data to improve locally the EGM geoid model so that accuracy of GPS in height determination can be improved.
ii. Accurate determination of geoid ellipsoid model in the area.
iii. Evaluation of GPS in difference in height determination.

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